MASON-MERCER

EXPANSION COMPENSATORS

& HOUSED EXPANSION JOINTS

> We are all interested in product development, but it is often difficult to trace. Let us share what we have learned.

When applying internally pressurized expansion joints, the designer has to be concerned with extension, compression, angular and torsional motion. Like automobile tires, rubber expansion joints are thick skinned forgiving creatures that tolerate abuse. Stainless steel is very reliable too, but only if expertly designed, properly anchored and guided. All of us have taken a strip of metal and bent it back and forth until it cracked and snapped. Multiple corrugations designed to low stresses eliminate the problem.

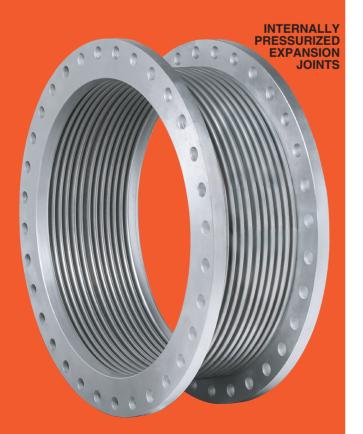
An anchor close to an expansion joint stabilizes one side. Then two guides, one 4 diameters from the joint and the other a minimum of 14 diameters from the first, lead the piping straight in and out. If the anchors are both up and down-stream, four guides are required, two on each side. Improper anchoring or guiding leads to failure. If major movements are required, it may become necessary to increase the outside diameter to prevent buckling. This increases both thrust and cost.

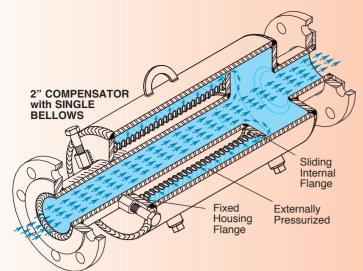
There is always the worry of personal injury from hot liquid or steam, even though the evolution from steel to galvanized steel, copper, bronze and finally stainless steel, has increased service life and operating pressures.

Some designer tried to solve some of these internally pressurized problems by telescoping two square housings around the joint. It reduced the rotational problem, but without the two external guides, the possibility of angular failure is always there.

Bulletin HEJ-31-1







Some years later there was a major change in concept. The industry turned to a completely housed construction. In this design, the bellows is welded to a sliding flange on the end of the piping, and to the fixed flange where the moving pipe enters. Unlike the old design, the fluid or gas surrounds the bellows so it is "Externally Pressurized". The design manuals say that a bellows is more stable when externally pressurized, but we have found no satisfactory explanation.

Self guiding is provided by the pipe passing through the opening on the one end and the small clearance of the moving flange **BELLOWS FAILURE** inside the outer housing. Should there be a bellows failure, the escape mananangan is only through the lower clearance, and back along the pipe rather than in an unpredictable direction. The housing is a great safety feature, **PATH OF FLUID** particularly in **OR STEAM IN FAILURE** steam lines.

For whatever reason, the entire industry refers to 2" movement designs as Expansion Compensators. They are shipped preset to allow for inward travel only in hot lines. Should there be a dual temperature situation, there is no engineering reason the compensator cannot be moved in 3/4" before installation, so it would accommodate 11/4" pipe expansion and 3/4" contraction or some other setting.

When the rated inward motion is increased to 4" or more, the industry name changes to Housed Expansion Joints, which is a much better description. "Expansion Compensator" is a function, not a product.

8"
HOUSED EXPANSION JOINT with MULTIPLE BELLOWS

Oddly enough, some people still describe the 2" movement Expansion Compensators as internally pressurized. They are not. Only the old design on page 1 is internally pressurized.

We had no illusions about coming up with a very different approach, but it is never our way to introduce a product without improvement. So just as we did with the straight hoses and Vees, we purchased twenty or thirty compensators and housed expansion joints from various manufacturers to see what was going on.

Perhaps the original engineer designed a whole range of consistent products. However, the more samples we looked at, the more confusing it became. There was no consistency. When people copy products to cheapen them or never completely understand the original design, the copy often suffers.

Virtually all manufacturers advertise 2" movement multi-ply bellows. Many companies just buy and resell without writing specs or testing. When their suppliers deliver single ply, the resale company would not know. There is no great harm, as the only reason to go to multiple plies is to increase pressure ratings without using a single thicker wall. A single thickness with the same corrugations and movements would suffer higher stresses, a shorter service life and the bellows would have a higher spring rate even though low spring rates are relatively unimportant. To maintain the same service life, the bellows would have to be longer to reduce movement per corrugation, and in addition to space considerations, more costly designs to manufacture.

Moving on to 4" and 8", most manufacturers use 2 ply, and some 3. The number is not particularly important. However, with greater movement, it becomes more difficult to maintain stability. Any stretched bellows is stable. However, pipelines do not only expand, they must cool and contract. When the motion is reversed and the bellows compressed, it can become unstable and buckle. Most manufacturers design to the maximum stable length and weld them to guide rings between sections to prevent buckling of a longer column.

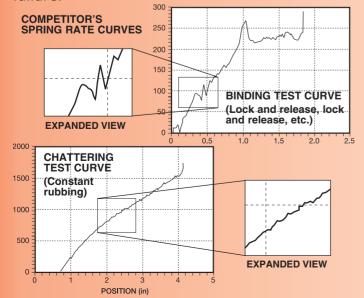
Our own designs vary from product to product, just depending on what works best. Since people like to know what they are buying, we note the number of bellows and plies for all products at this writing. Most companies do not.

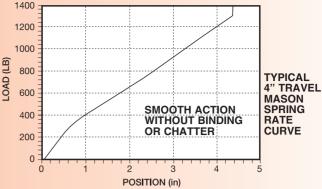
We found that to prevent buckling, some manufacturers had their bellows rubbing against the inside pipe or the outer shell. It would seem they must wear through and leak earlier, so tight fits are a poor way to go. (See bronze bellows photo on page 3)

Others went to huge outer housings as compared to the inner pipe, so their products were clumsy (below). In our own designs, we have succeeded in providing good working clearances, both between the inside of the bellows and the moving pipe as well as the outer shell. We note clearances on all product drawings. Competitors do not. (See pages 6 through 11)

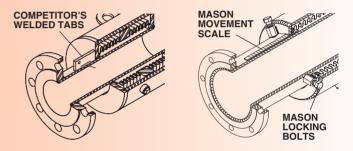


In checking spring rates, we found that some competitors are so concerned with alignment, that clearances between the moving pipe and the entry collar as well as the moving inner flange, and the outer shell were so tight that binding was a serious problem. We are publishing a few test curves to show this condition. Since there is no need for so small a tolerance, our clearances are roomier for smoother travel, as shown by the Mason test curve at the top of the next column. When expansion joints bind, it increases the anchorage loads. Binding intermediate rings stretch bellows unevenly and can cause failure.





Another improvement is our introducing locking bolts to maintain the installed position. All of the other manufacturers use welded tabs. The tabs are knocked out after the piping is fixed to the expansion joint. Sometimes they are flimsy and fall off. More importantly, the side welds are often within the movement of the pipe entering the housing. The weld has to tear its way through until it clears. Not the smooth motion we would all like to have.

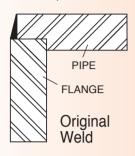


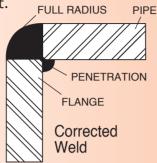
Perhaps our most interesting contribution is the introduction of a scale to confirm the starting position is zero for the average installation. Many of the stop-tabbed samples we checked weré not. When the joint is in service, the scale indicates how much the pipe has expanded and how much the bellows have been extended. In a hot and cold situation, you can loosen the restraining bolts, and push the bellows to the desired starting position to allow for a line cooling down or a seasonal change in temperature. Reading the scale makes it easy. Re-lock the bolts and continue with the installation. (Note: the 2" movement expansion compensators have a 0, 1" and 2" reference only.)

If for whatever reason you have to remove an expansion joint temporarily, you can retighten the locking bolts, remove it, do the maintenance work and reinstall the expansion joint without fighting it into position as you would have to with any other device. Loosen the bolts and it is back in service. Welded tabs would have been long gone. While any good mechanic can find a way, this is much easier.

Shortly after we sold our first housed expansion joints, we had a serious failure even before they were put into service. One of our contractors was prefabbing as much as possible to minimize time on the jobsite. Rather than installing the housed expansion joint between pipe ends in the field, he welded long extensions to the pipe on both

sides. In normal rough handling, one of the modified joints was dropped. The cantilever of the long welded pipe snapped the flange off the fixed end. When we got it back in the shop, we found the method we were using in machining the flange to the I.D. of the housing left a small lip around the pipe perimeter as sketched. This undersized weld looked great and would have held the pressure, but not impact.





Here again, we checked competitor's products, and found our original technique was typical. We re-examined all of our welds and changed every one to good piping practice with welds as sketched. Maybe this is overkill, but neither you nor we will ever suffer a weld failure again and that's good to know.

Earlier we suggested the bellows spring rate was insignificant. The reason is the thrust from a housed expansion joint is equal to the area as calculated to about the center of the bellows multiplied by the pressure in the pipe line. Typically a 4" pipe bellows might have a 61/4" diameter to the center of the corrugation. At 225 psi the thrust force is a nominal 6900 lbs. The spring rate of our 4" travel HEJ is 300 lbs. per inch. The 8" HEJ is 150 lbs. per inch. Therefore, with either joint the total bellows resistance at 4" or 8" travel is 1200 lbs. This increases the anchor load to 6900 plus 1200 lbs. or 8100 lbs. total. 1200/8100 =15%. If a competitive product were half as stiff, the anchorage requirement would drop to 7500 lbs. If twice as stiff, it would increase to 9300 lbs. In the real world, when designing an anchor, all these numbers are in the same order of magnitude. The spring force is relatively insignificant, except for an extremely unusual installation where there might be concern for buckling of copper pipe or something of that nature.

SAFETY FACTOR

Our last worry was the question of safety factor.

A flexible hose or internally pressurized expansion joint fails because the walls fail in tension beyond a given pressure. Since all housed expansion joints are pressurized externally, that is not the phenomena. The pressure on the outside eventually forces the

corrugations to squirm and become distorted until they collapse completely, as shown by one of our test photographs.

According to the standards established by The Stainless Steel Expansion Joint Institute, an expansion joint is considered safe when this collapse occurs at 2.25 times the working pressure. That means the safety factor is only 2.25. Most manufacturers do not publish their collapse ratios, but a 2.25 safety factor seemed very low. Braided hoses have safety factors between 3 and 4. Why is 2.25 acceptable in an expansion joint?

Flexible products are always riskier than solid pipe, so it seemed only right that our housed expansion joints and expansion compensators should have a **safety factor** between **3.5** and **4** as published and what we have worked to in all designs.

All expansion joints are more subject to collapse, when fully extended. Our ratings are all at full extension. In many cases the collapse may take place without leakage. However, when the pipe system cools down and the cycle reverses, the collapsed area is crushed and dramatic leakage follows. Should it turn out our spring rates are higher than some of our competitors, it is because of our safer bellows construction. Safety is far more important than spring rate.

We have an elaborate test facility to test Mercer Rubber Expansion Joints and all Stainless Steel products. All product designs are thoroughly tested before marketing. Unfortunately, our tests show design ratings by competitors are often optimistic. Testing rather than theoretical design is the only answer.

Spring Rate Test in Progress





Hydro Pressure Test in Progress

If you have never had a problem with an expansion compensator or housed expansion joint, everything we have discussed may seem unimportant. However, our improvements will keep both of us out of trouble and make life easier. Let's review.

Mason Improvements

- Good operating clearances to prevent binding.
- 2. A much better locking mechanism that can be used to partially compress joints prior to installation to allow for contraction as well as expansion on installations with temperatures below ambient when in service. The locking device is a permanent part of the construction. They can always be tightened to hold the expansion joint in a particular position for removal while piping is serviced.
- 3. A depth gauge on the moving end to monitor movements, make certain that joints are at the 0 position before installation, or used to pre-set joints in some preferred position.
- Great attention to canister and pipe welding details.
- 5. Internal and external clearances to prevent bellows wear because of rubbing.
- 6. Safety factors between 3.5 and 4, compared to others at 2.25. Double drains on most

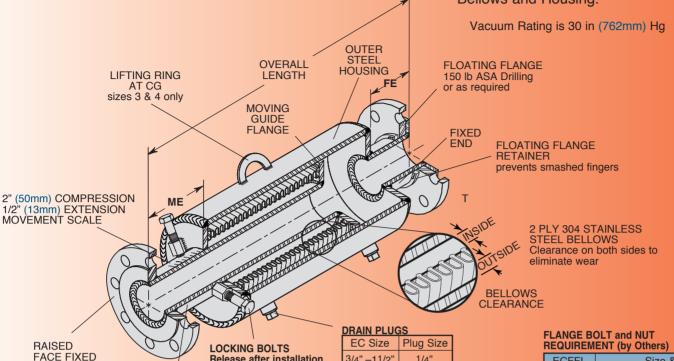
- designs, generous lifting near the center of gravity for easier handling.
- 7. A raised face flange and a floating flange on all flanged products for easier installation and bellows anti-torquing protection.
- 8. Grooved fittings are beveled as well to allow welding into pipe lines as an alternate method. (Mason does not recommend welding.)
- 9. Our staff of in-house engineers holding licenses in virtually all of the States with the capability to design or review complete piping systems when our clients need those services. We will try to help you in any case should you have bought from others that offer no engineering service. Seismic problems can be addressed as well.

If the following tables of externally pressurized stock items do not meet all of your requirements, please let us offer custom product. We also manufacture internally pressurized products and welcome inquiries on these as well. We are here to help.

Thanks for bearing with me.

Marron & Mason Bresiden

Norman J. Mason, President



CARBON STEEL PLATE

FLANGE

150 lb ASA

as required

Drilling or

LANGE III	IOIKINESS			
		Flange		
Pipe	Thickness T			
(in)	(mm)	(in) (mm)		
3/4 thru 4	20 thru 100	5/8 16		

PRESSURE REDUCTION TABLE

3/4" -11/2'

3/8"

1/2

2" - 3"

Release after installation

Bolt No & Size

2 - 3/8"

2 - 1/2

3 - 5/8"

EC Size

3/4" - 2'

21/2" - 3

4"

MOVING

END

Temperature (°F) (°C)	Rated Pressure (psi)(kg/cm²)
200 93	182 12.8
250 121	176 12.4
300 149	170 12.0
400 204	156 11.0
500 260	154 10.8
600 316	142 10.7
700 371	148 10.4
800 427 N	lot Recommended

		,
ECFFL Size	Quantity	Size & Length
3/4 1 11/4 11/2 2 & 21/2 3 4	8 8 8 8 8 8	1/2 x 21/2 1/2 x 21/2 1/2 x 21/2 1/2 x 21/2 1/2 x 23/4 5/8 x 3 5/8 x 31/4 5/8 x 31/4

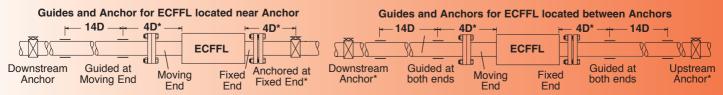
INSERT FLANGE BOLTS AS SHOWN



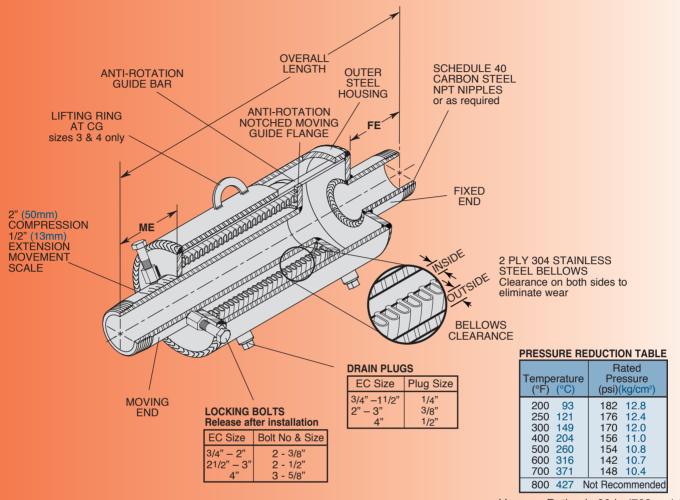
Type & Size	Pipe Size (in) (mm)	Overall Length (in) (mm)	ME Moving End Neutral Length (in) (mm)	FE Fixed End Length (in) (mm)	Outer Housing O.D. (in) (mm)		Bellows rance Outside (in) (mm)	$\begin{array}{c} \text{Spring} \\ \text{Rate} \\ \left(\frac{\text{lbs}}{\text{in}} \right) \left(\frac{\text{kg}}{\text{cm}} \right) \end{array}$	Thrust [†] @ 200 13.8 psi bar (lbs) (kg)	Rated Pressure @70°F @21°C (psi) (kg/cm²)	Ship Wt. (lbs)(kg)
ECFFL-3/4		121/2 318	31/2 89	13/4 44	27/8 73	0.10 3	0.43 11	89 16	350 159	200 14	11 5
ECFFL-1		121/2 318	31/2 89	13/4 44	31/2 89	0.13 3	0.55 14	95 17	500 227	200 14	14 6
ECFFL-11/4		13 330	33/4 95	2 51	4 102	0.15 4	0.47 12	103 18	800 363	200 14	15 7
ECFFL-11/2		13 330	33/4 95	2 51	41/2 114	0.17 4	0.46 12	106 19	1100 499	200 14	19 9
ECFFL-2	2 50	131/2 343	41/8 105	21/8 54	51/4 133	0.17 4	0.52 13	110 20	1600 726	200 14	24 11
ECFFL-21/2	21/2 65	141/4 362	41/4 108	21/4 55	61/4 159	0.24 6	0.53 14	126 23	2400 1089	200 14	35 16
ECFFL-3	3 80	143/4 375	41/2 115	21/2 65	65/8 168	0.32 8	0.37 9	140 25	3500 1588	200 14	47 21
ECFFL-4	4 100	143/4 375	41/2 115	21/2 65	85/8 219	0.33 8	0.81 21	150 27	5200 2359	200 14	70 32

*Lower Thrust Forces in proportion at lower pressures, i.e. 100 psi Force = 100/225 x published Thrust. Forces on Pipe Anchors must include Thrust Force and Spring Force. Spring Force is determined by multiplying the joint Spring Rate by its Thermal Movement (in/mm).

GUIDE SPACING - Referencing Pipe Diameter "D"



^{*}Plus an additional 3" (76mm) for Sizes 3/4 to 21/2



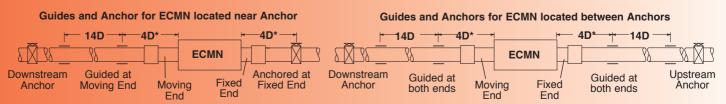
Vacuum Rating is 30 in (762mm) Hg

E	ECMN DIMENSIONS AND PRESSURE RA	TINGS (Britis	sh & Metric	: Units) 2'	" (50m	m) COMPRES	SION, 1/2" ((13mm)	EXTENSI	ON
- 6										

Type & Size	Pipe Size (in) (mm)	Overall Length (in) (mm)	ME Moving End Neutral Length (in) (mm)	FE Fixed End Length (in) (mm)	Outer Housing O.D. (in) (mm)		I Bellows rance Outside (in) (mm)	$\begin{array}{c} \text{Spring} \\ \text{Rate} \\ \left(\frac{ \text{bs} }{\text{in}} \right) \left(\frac{\text{kg}}{\text{cm}} \right) \end{array}$	Thrust [†] @ 200 13.8 psi bar (lbs) (kg)	Rated Pressure @70°F @21°C (psi) (kg/cm²)	
ECMN-3/4	3/4 20	121/2 318		15/8 40	27/8 73	0.10 3	0.43 11	89 16	350 159	200 14	7 3
ECMN-1	1 25	121/2 318		15/8 40	31/2 89	0.13 3	0.55 14	95 17	500 227	200 14	10 4
ECMN-11/4	11/4 32	13 330		17/8 46	4 102	0.15 4	0.47 12	103 18	800 363	200 14	11 5
ECMN-11/2	11/2 40	13 330		17/8 46	41/2 114	0.17 4	0.46 12	106 19	1100 499	200 14	13 6
ECMN-2	2 50	131/2 343		21/8 53	51/4 133	0.17 4	0.52 13	110 20	1600 726	200 14	16 7
ECMN-21/2	21/2 65	141/4 362		21/4 55	61/4 159	0.24 6	0.53 14	126 23	2400 1089	200 14	23 10
ECMN-3	3 80	143/4 375		21/2 65	65/8 168	0.32 8	0.37 9	140 25	3500 1588	200 14	32 15
ECMN-4	4 100	143/4 375		21/2 65	85/8 219	0.33 8	0.81 21	150 27	5200 2359	200 14	50 23

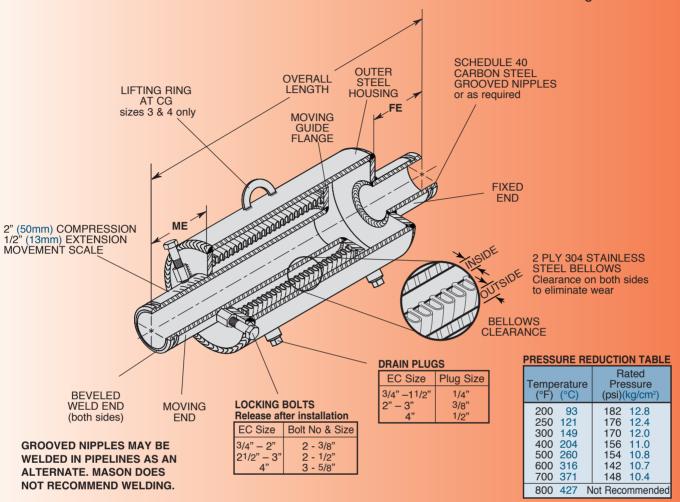
Lower Thrust Forces in proportion at lower pressures, i.e. 100 psi Force = 100/225 x published Thrust. Forces on Pipe Anchors must include Thrust Force and Spring Force. Spring Force is determined by multiplying the joint Spring Rate by its Thermal Movement (in/mm).

GUIDE SPACING - Referencing Pipe Diameter "D"



^{*}Plus an additional 3" (76mm) for Sizes 3/4 to 21/2





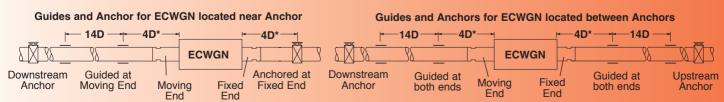
Vacuum Rating is 30 in (762mm) Hg

ECWGN DIMENSIONS AND PRESSURE RATINGS (British & Metric Units) 2" (50mm) COMPRESSION, 1/2" (13mm) EXTENSION

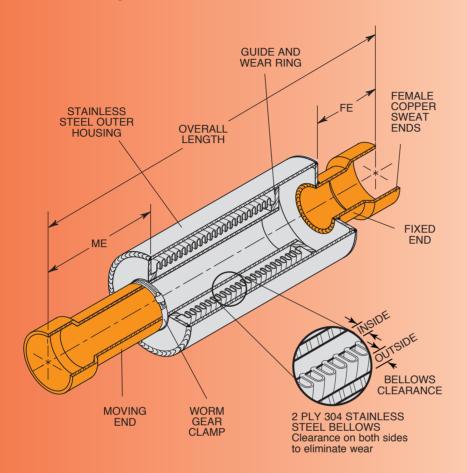
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Type & Size	Pipe Size (in) (mm)	Overall Length (in) (mm)	ME Moving End Neutral Length (in) (mm)	FE Fixed End Length (in) (mm)	Outer Housing O.D. (in) (mm)		Bellows rance Outside (in) (mm)	$\begin{array}{c} \text{Spring} \\ \text{Rate} \\ \frac{\text{ bs }}{\text{in}} \begin{pmatrix} \underline{\text{kg}} \\ \text{cm} \end{pmatrix} \end{array}$	Thrust [†] @ 200 13.8 psi bar (lbs) (kg)	Rated Pressure @70°F @21°C (psi) (kg/cm²)	
ECWGN-3/4 ECWGN-1 ECWGN-11/4 ECWGN-11/2	3/4 20 1 25 11/4 32 11/2 40	121/2 318 121/2 318 13 330 13 330	33/4 95	15/8 40 15/8 40 17/8 46 17/8 46	27/8 73 31/2 89 4 102 41/2 114	0.10 3 0.13 3 0.15 4 0.17 4	0.43 11 0.55 14 0.47 12 0.46 12	89 16 95 17 103 18 106 19	350 159 500 227 800 363 1100 499	200 14 200 14 200 14 200 14	7 3 9 4 10 5 13 6
ECWGN-2 ECWGN-21/2 ECWGN-3 ECWGN-4	2 50 21/2 65 3 80 4 100	131/2 343 141/4 362 143/4 375 143/4 375	43/8 110 41/2 115	21/4 55 21/4 55 21/2 65 21/2 65	51/4 133 61/4 159 65/8 168 85/8 219	0.17 4 0.24 6 0.32 8 0.33 8	0.52 13 0.53 14 0.37 9 0.81 21	110 20 126 23 140 25 150 27	1600 726 2400 1089 3500 1588 5200 2359	200 14 200 14 200 14 200 14	17 8 24 11 33 15 50 23

[†]Lower Thrust Forces in proportion at lower pressures, i.e. 100 psi Force = 100/225 x published Thrust. Forces on Pipe Anchors must include Thrust Force and Spring Force. Spring Force is determined by multiplying the joint Spring Rate by its Thermal Movement (in/mm).

GUIDE SPACING - Referencing Pipe Diameter "D"



^{*}Plus an additional 3" (76mm) for Sizes 3/4 to 21/2



INSTALLATION:

- Thoroughly clean male and female ends using steel wool and steel brushes.
- 2. Apply flux.
- 3. Heat joint for proper flow of silver solder. Silver solder flows around 430°F. Composition is silver and tin only. There should be no lead content.
- Do not use brazing rod or other high temperature techniques. Overheating will cause leaks.
- 5. Remove Worm Gear Clamp.

PRESSURE REDUCTION TABLE

Temperature (°F) (°C)	Rated Pressure (psi)(kg/cm²)
150 66 300 149	160 11 145 10
400 204	135 9

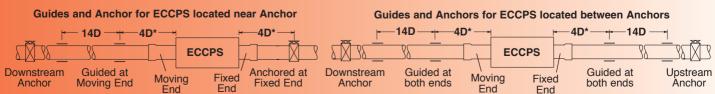
Vacuum Rating is 30 in (762mm) Hg

ECCPS DIMENSIONS AND PRESSURE RATINGS (British & Metric Units) 2" (50mm) COMPRESSION, 1/2" (13mm) EXTENSION

Type & Size	Tubing Size ^{††} (in) (mm)	Overall Length (in) (mm)	ME Moving End Neutral Length (in) (mm)	FE Fixed End Length (in) (mm)	Outer Housing O.D. (in) (mm)		I Bellows rance Outside (in) (mm)	$\begin{array}{c} \text{Spring} \\ \text{Rate} \\ \left(\frac{ \text{bs}}{\text{in}} \right) \left(\frac{\text{kg}}{\text{cm}} \right) \end{array}$	Thrust ⁺⁺ @ 200 13.8 psi bar (lbs) (kg)	Rated Pressure @70°F @21°C (psi) (kg/cm²)	
ECCPS-3/4		111/2 292	31/8 79	15/8 40	2 51	0.17 4	0.11 3	23 4	320 145	200 14	2 1
ECCPS-1		111/2 292	31/8 79	15/8 40	2 51	0.22 6	0.13 3	44 8	520 236	200 14	2 1
ECCPS-11/2		12 305	31/2 89	13/4 44	23/4 70	0.20 5	0.22 6	50 9	630 286	200 14	3 2
ECCPS-11/2		12 305	31/2 89	13/4 44	23/4 70	0.17 4	0.20 5	98 18	750 340	200 14	4 2
ECCPS-2	2 50	121/4 311	33/4 95	13/4 44	31/2 89	0.16 4	0.13 3	168 30	1160 526	200 14	5 2
ECCPS-21/2	2 21/2 65	131/4 337	41/4 108	21/8 54	4 102	0.20 5	0.22 6	195 35	1810 821	200 14	6 3
ECCPS-3	3 80	131/4 337	41/4 108	21/8 54	41/4 114	0.21 5	0.28 7	316 57	2440 1107	200 14	7 3
ECCPS-4	4 100	141/2 368	43/8 111	21/2 65	6 150	0.14 4	0.30 8	350 63	3700 1678	200 14	25 11

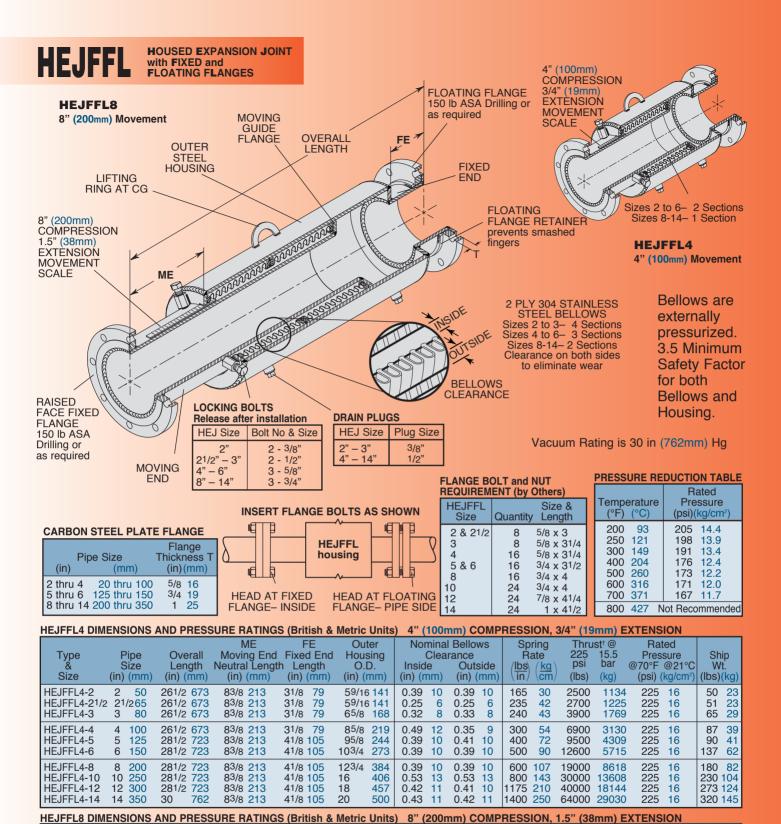
^{††}Female end fits over copper tubing, e.g. 11/2" (40mm) fits over 11/2" (40mm) tubing.

GUIDE SPACING – Referencing Pipe Diameter "D"



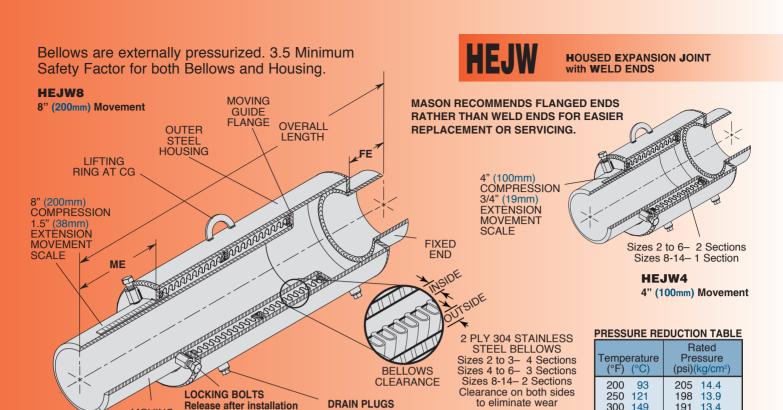
^{*}Plus an additional 3" (76mm) for Sizes 3/4 to 21/2

^{*}Lower Thrust Forces in proportion at lower pressures, i.e. 100 psi Force = 100/225 x published Thrust. Forces on Pipe Anchors must include Thrust Force and Spring Force. Spring Force is determined by multiplying the joint Spring Rate by its Thermal Movement (in/mm).



Nominal Bellows ME Outer Spring Thrust[†] @ Rated Moving End Fixed En Neutral Length Length Fixed End Rate Overall Housing Clearance Pressure Ship Type & Wt. Length har Size O.D. Inside Outside /lbs\ (kg cm @70°F (psi) (kg/cm² Size (in) (mm) (in) (mm) (in) (mm) (in) (mm) (in) (mm) (in) (mm) (in) (mm (in) (lbs) (kg) (lbs)(kg) 43 1092 HEJFFL8-2 50 107/8 276 31/8 79 59/16 141 0.39 10 0.39 10 83 15 2500 1134 225 16 50 23 107/8 276 21 22 23 HEJFFL8-21/2 21/265 43 1092 31/8 79 59/16 141 0.25 6 0.25 6 118 2700 1225 225 16 51 29 HEJFFL8-3 3 80 43 1092 107/8 276 31/8 79 65/8 168 0.32 8 0.33 8 120 3900 1769 225 16 65 HEJFFL8-4 4 100 43 1092 107/8 276 31/8 79 85/8 219 0.49 12 0.35 9 150 27 6900 3130 225 16 87 39 HEJFFL8-5 47 1194 127/8 327 41/8 105 95/8 244 0.39 36 225 125 10 0.41 10 200 9500 4309 16 90 41 103/4 273 250 225 HFJFFI 8-6 6 150 47 1194 127/8 327 41/8 105 0.39 10 0.39 45 12600 5715 137 62 10 16 HEJFFL8-8 8 200 47 1194 127/8 327 41/8 105 123/4 384 0.39 10 0.39 10 300 54 19000 8618 225 16 180 82 230 104 HEJFFL8-10 10 250 47 1194 127/8 327 41/8 105 16 406 0.53 13 0.53 13 400 72 30000 13608 225 16 588 HEJFFL8-12 12 300 47 1194 127/8 327 41/8 105 0.42 0.41 105 40000 18144 225 273 124 18 457 10 16 HEJFFL8-14 14 350 50 1270 127/8 327 41/8 105 20 500 0.43 11 0.42 700 125 64000 29030 225

¹Lower Thrust Forces in proportion at lower pressures, i.e. 100 psi Force = 100/225 x published Thrust. Forces on Pipe Anchors must include Thrust Force and Spring Force. Spring Force is determined by multiplying the joint Spring Rate by its Thermal Movement (in/mm).



HEJW4 DIMENSIONS AND PRESSURE RATINGS (British & Metric Units) 4" (100mm) COMPRESSION, 3/4" (19mm) EXTENSION

HEJ Size

2" - 3" 4" - 14"

Type & Size	Pipe Size (in) (mm)	Overall Length (in) (mm)	ME Moving End Neutral Lengt (in) (mm)		Outer Housing O.D. (in) (mm)		I Bellows rance Outside (in) (mm)	Spring Rate (<u>lbs</u>) (<u>kg</u>)	Thrust [†] @ 225 15.5 psi bar (lbs) (kg)	Rated Pressure @70°F @21°C (psi) (kg/cm²)	Ship Wt. (lbs)(kg)
HEJW4-2 HEJW4-21/2 HEJW4-3	2 50 21/265 3 80	22 559 22 559 22 559	51/2 140 51/2 140 51/2 140	11/2 38 11/2 38 11/2 38	59/16 141 59/16 141 65/8 168	0.39 10 0.25 6 0.32 8	0.39 10 0.25 6 0.33 8	165 30 235 42 240 43	2500 1134 2700 1225 3900 1769	225 16 225 16 225 16	50 23 51 23 65 29
HEJW4-4 HEJW4-5 HEJW4-6	4 100 5 125 6 150	241/2 622 241/2 622 241/2 622	6 152 6 152 6 152	11/2 38 21/2 64 21/2 64	85/8 219 95/8 244 103/4 273	0.49 12 0.39 10 0.39 10	0.35 9 0.41 10 0.39 10	300 54 400 72 500 90	6900 3130 9500 4309 12600 5715	225 16 225 16 225 16	87 39 90 41 137 62
HEJW4-8 HEJW4-10 HEJW4-12 HEJW4-14	8 200 10 250 12 300 14 350	241/2 622 241/2 622 241/2 622 26 660	6 152	21/2 64 21/2 64 21/2 64 21/2 64	123/4 384 16 406 18 457 20 500	0.39 10 0.53 13 0.42 11 0.43 11	0.39 10 0.53 13 0.41 10 0.42 11	1175 210	19000 8618 30000 13608 40000 18144 64000 29030	225 16 225 16 225 16 225 16	180 82 230 104 273 124 320 145

Plug Size

3/8

1/2

Vacuum Rating is

30 in (762mm) Hg

400 204

600

500 260

700 371

800 427

316

12.4

12.0

173 12.2

Not Recommended

176

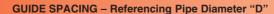
171

167 11.7

HEJW8 DIMENSIONS AND PRESSURE RATINGS (British & Metric Units	8" (200mm) COMPRESSION, 1.5" (38mm) EXTENSION
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Type & Size	Pipe Size (in) (mm)	Overall Length (in) (mm)	ME Moving E Neutral Le (in) (mm	ngth Length	Outer Housing O.D. (in) (mm)		Bellows rance Outside (in) (mm)	$\begin{array}{c} \text{Spring} \\ \text{Rate} \\ \left(\begin{array}{c} \underline{\text{lbs}} \\ \overline{\text{in}} \end{array} \right) \left(\begin{array}{c} \underline{\text{kg}} \\ \overline{\text{cm}} \end{array} \right) \end{array}$	Thrust [†] @ 225 15.5 psi bar (lbs) (kg)	Rated Pressure @70°F @21°C (psi) (kg/cm²)	
HEJW8-2 HEJW8-21/2 HEJW8-3	2 50 21/265 3 80	40 1016 40 1016 40 1016	91/2 24	1 11/2 38	59/16 141 59/16 141 65/8 168	0.39 10 0.25 6 0.32 8	0.39 10 0.25 6 0.33 8	83 15 118 21 120 22	2500 1134 2700 1225 3900 1769	225 16 225 16 225 16	50 23 51 23 65 29
HEJW8-4 HEJW8-5 HEJW8-6	4 100 5 125 6 150	40 1016 421/2 1080 421/2 1080	91/2 24 10 254 10 254	4 21/2 64	85/8 219 95/8 244 103/4 273	0.49 12 0.39 10 0.39 10	0.35 9 0.41 10 0.39 10	150 27 200 36 250 45	6900 3130 9500 4309 12600 5715	225 16 225 16 225 16	87 39 90 41 137 62
HEJW8-8 HEJW8-10 HEJW8-12 HEJW8-14	8 200 10 250 12 300 14 350	421/2 1080 421/2 1080 421/2 1080 451/2 1156	10 254 10 254 10 254 10 254	1 21/2 64 1 21/2 64	123/4 384 16 406 18 457 20 500	0.39 10 0.53 13 0.42 11 0.43 11	0.39 10 0.53 13 0.41 10 0.42 11	300 54 400 72 588 105 700 125	19000 8618 30000 13608 40000 18144 64000 29030	225 16 225 16 225 16 225 16	180 82 230 104 273 124 320 145

[†]Lower Thrust Forces in proportion at lower pressures, i.e. 100 psi Force = 100/225 x published Thrust. Forces on Pipe Anchors must include Thrust Force and Spring Force. Spring Force is determined by multiplying the joint Spring Rate by its Thermal Movement (in/mm).



MOVING

END

BEVELED

WELD ENDS

HEJ Size

4" - 6"

8" - 14

21/2" - 3'

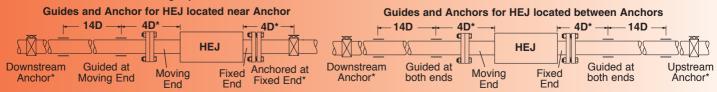
Bolt No & Size

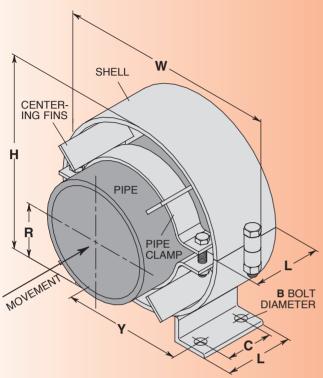
2 - 3/8

2 - 1/2"

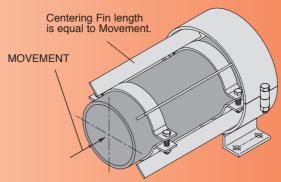
3 - 5/8"

3 - 3/4"





Typical AA through FF One Clamp Configuration



Typical GG through PP Two Clamp Configuration

SPG SHELL SELECTION TABLE for 4" (100mm), 6" (150mm) & 8" (200mm) MOVEMENT

		Max.						
Pipe		Standard						
Size	1"	11/2"	2"	21/2"	3"	31/2"	4"	Mvmt.±*
(in)(mm)	25mm	32mm	50mm	65mm	80mm	90mm	100mm	(in)(mm)
1/2 15	AA	AA	BB	DD	DD	DD	EE	4 100
3/4 20	AA	BB	CC	DD	DD	EE	EE	4 100
1 25	AA	BB	CC	DD	DD	EE	EE	4 100
11/4 32	AA	BB	CC	DD	DD	EE	EE	4 100
11/2 40	BB	BB	CC	DD	DD	EE	EE	4 100
2 50	BB	CC	DD	DD	EE	EE	FF	4 100
21/2 65	CC	CC	DD	DD	EE	EE	FF	4 100
3 80	CC	DD	DD	EE	FF	FF	_FF	4 100
4 100	DD	DD	EE	EE	FF	FF	GG	6 150
5 125	EE	EE	EE	FF	FF	GG	HH	6 150
6 150	EE	EE	FF	FF	GG	HH	HH	6 150
8 200	FF	FF	GG	HH	HH	JJ	JJ	6 150
10 250	HH	HH	НН	JJ	JJ	KK	KK	6 150
12 300	JJ	JJ	JJ	KK .	KK	LL	LL	8 150
14 350	KK	KK	KK	KK	LL	LL	MM	8 150
16 400	LL	LL	LL	LL	MM	MM	NN	8 150
18 450	MM	MM	MM	MM	NN	NN	NN	8 150
20 500	NN	NN	NN	NN	PP	PP	PP	8 150
24 600	PP	PP	PP	PP	_	_	_	8 150

^{*}Centering Fin length is equal to the Maximum Standard Movement. Non-standard movements are available.

SPG DIMENSIONS (inches)

SFG DIMENSIONS (INCHES)									
Type	Shell Code	Н	R	W	Υ	В	С	L	
SPG	AA	57/8	31/ <u>2</u>	61/8	41/8	5/8	13/4	3	
SPG	BB	63/4	4	71/8	43/8	5/8	13/4	3	
SPG	CC	75/8	43/8	81/8	51/8	5/8	13/4	3	
SPG	DD	91/4	51/4	101/8	61/8	5/8	13/4	3	
SPG	EE	115/8	61/4	121/8	7	5/8	23/4	4	
SPG	FF	133/8	7	141/8	81/4	5/8	23/4	4	
SPG	GG	15 ¹ /8	77/8	16 ¹ /8	97/8	3/4	4	6	
SPG	HH	17	87/8	18 ¹ /8	107/8	3/4	4	6	
SPG	JJ	18 ³ /4	93/4	20 ¹ /8	117/8	3/4	4	6	
SPG	KK	21	10 ⁷ /8	221/8	11 ³ / ₄	3/4	6	8	
SPG	LL	23 ¹ /8	12 ¹ /8	241/8	14 ¹ / ₂	7/8	6	8	
SPG	MM	25	13	261/8	15 ¹ / ₂	7/8	6	8	
SPG	NN	273/4	143/4	281/8	171/8	11/8	6	8	
SPG	PP	311/2	16 ¹ /2	321/8	191/4	11/8	6	8	

SPG DIMENSIONS (mm)

Туре	Shell Code	Н	R	W	Υ	В	С	L
SPG	AA	149	90	156	104	16	44	76
SPG	BB	171	102	181	111	16	44	76
SPG	CC	194	111	206	130	16	44	76
SPG	DD	235	133	257	156	16	44	76
SPG	EE	295	159	308	178	16	70	102
SPG	FF	340	178	360	210	16	70	102
SPG	GG	384	200	410	251	19	102	152
SPG	HH	432	225	460	276	19	102	152
SPG	JJ	476	248	511	302	19	102	152
SPG	KK	533	276	562	298	19	152	203
SPG	LL	587	308	613	368	22	152	203
SPG	MM	635	330	664	394	22	152	203
SPG	NN	705	375	714	435	22	152	203
SPG	PP	800	419	816	489	22	152	203



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